

METHOD AND APPARATUS OF UTILIZING RF/MICROWAVE
AND OPTICAL MIXING TECHNIQUES TO SELECT A GIVEN BAND
5 OF AN OPTICAL TRANSMISSION

Field of the Invention

The field of the invention relates to optical
communications systems and, more particularly, to opto-
10 electronic systems for fiber optic communications
networks.

Background of the Invention

Methods of transmitting and receiving
15 communications signals over fiber optic networks are
known. RF subcarrier division multiplexed (SDM)
transmission techniques are also known. Such techniques
have been applied to a variety of communications
networks, including hybrid fiber optic/coaxial cable
20 (HFC) networks for community antenna television (CATV)
distribution. In fact subcarrier division multiplexing
is the standard multiplexing technique used in CATV
networks today.

The prior use of subcarrier division multiplexing
25 techniques in HFC networks has generally limited the
optical bandwidth utilized for the transmission to that
of the coaxial cable portion of the network (e.g. 50-
750 MHz). This makes sense for the analog amplitude
modulation-vestigial sideband (AM-VSB) transmission of
30 television signals where the linearity of the optical
system creates an upper limit on the number of
subcarrier multiplexed channels that can be transmitted

with the required signal quality over the fiber optic portion of the network. Thus, such network implementations benefit from the low loss of the fiber, but fail to exploit the significant bandwidth of the fiber in the distribution of communications signals and services.

Key to the teachings of the prior art has been a belief that the bandwidth of the coaxial cable portion of the network somehow limits the laser bandwidth that can be effectively utilized to deliver services over such a hybrid network. The current industry trend is to provide allocated bandwidth services over the HFC network for applications such as internet, pay per view and telephone. These allocated bandwidth services typically have taken the form of a digital quadrature amplitude modulation (QAM) and do not require the same degree of linearity from the optical system as the AM-VSB signals have required in the past. This fact is generally known, but it is not effectively exploited in modern CATV network architectures.

The substantially relaxed linearity specifications that result from the utilization of digital QAM signals in contrast to the AM-VSB signals can impact the network architecture by two distinctly separate means. One such means is by the wavelength division multiplexing (WDM) of several laser wavelengths, each of which carries an SDM signal containing multiple QAM subcarriers. Since the linearity specifications are somewhat relaxed, these WDM signals can be transmitted over a single fiber provided that the wavelengths are separated at the hub by an optical wavelength division demultiplexing filter prior to combining one of these

wavelengths with the optical carrier containing the SDM AM-VSB signals. These two wavelengths can thereafter be transmitted a reasonable distance through the fiber while maintaining the linearity performance required by
5 the AM-VSB system.

It is important to note that in such WDM systems containing SDM digital QAM signals on the optical wavelengths, the prior art has taught the utilization of the RF bandwidth ranging from 550-750 MHz. The RF
10 bandwidth ranging from 50-550 MHz is reserved for the SDM AM-VSB signals, and the upper bandwidth limit of 750 MHz is imposed by the transmission features of the coaxial cable (and its associated RF amplifier chain). Therefore a mere 200 MHz of optical bandwidth is
15 utilized for the SDM QAM signals. However there is no fundamental reason why such bandwidth should be so limited. This is a restriction imposed by the coaxial cable system, not by the optical system.

The above scenario considers an analog system that
20 carries a combination of AM-VSB signals and QAM signals on the multiplexed analog subcarriers. However, these considerations are equally pertinent to the digital communications system. The main difference is that in the case of the digital system, bandwidth is increased
25 by time division multiplexing (TDM) of multiple digital signals, whereas in the analog system bandwidth is increased by subcarrier division multiplexing of analog subcarriers.

In the digital system the prior art has taught two
30 distinct techniques whereby additional optical bandwidth may be utilized. One such technique comprises the utilization of multiple optical wavelengths and WDM

technology. The other technique comprises increasing the bit rate of the TDM signal. Both of these methodologies require substantial upgrades to the network terminal equipment in order to enable the
5 utilization of additional optical bandwidth.

Accordingly it is an object of this invention to provide a means for increasing the utilization of optical spectrum in the fiber optic portion of the network with the minimum impact on the network terminal
10 equipment.

It is a further object of this invention to provide a means for distributing the additional bandwidth created by increasing the utilization of optical spectrum to different portions of the
15 electrical (or optical) network where less total bandwidth is required.

It is a further object of this invention to provide additional utility to the network by enabling the portion of the bandwidth that is to be distributed
20 to a given portion of the network to be remotely selectable by RF and/or optical techniques.

Summary of the Invention

A method and apparatus are provided for
25 transmitting and receiving multiple RF/microwave subcarriers on a single optical wavelength over an optical link. The method includes the steps of modulating a plurality of RF/microwave subcarrier frequencies with a respective communication signal and
30 modulating an optical carrier wave with the plurality of modulated RF/microwave subcarrier frequencies. The method further includes the steps of detecting the

plurality of RF/microwave subcarriers of the optical carrier wave and mixing those subcarriers with a first local oscillator (LO) frequency to create a new heterodyne IF frequency above the highest frequency component of the modulated signal spectrum of the detected subcarriers, filtering an RF/microwave subcarrier frequency of the plurality of detected RF/microwave subcarriers utilizing a bandpass filter at an IF center frequency of the new IF frequency and mixing the filtered RF/microwave subcarrier with a second local oscillator (LO) frequency to derive a difference frequency at a desired center frequency for propagation over the subsequent network element.

Further the disclosed method utilizes RF/microwave (and/or optical heterodyne) mixing techniques to select a given band of frequencies from an optical transmission and thereafter to distribute the selected band over a portion of the network. The method includes the modulation of multiple communications signals (e.g. TDM or SDM) on multiple RF (or microwave) carriers on a single optical wavelength (or multiple optical wavelengths). The method further includes the step of detecting the set of multiple communications signals on multiple frequency bands and then selecting one of the detected bands for distribution over a portion of the network.

In the general case where the transmitted component carries high frequency microwave signals that are outside of the bandwidth of the detector system, the method further includes the step of selecting one (or more) of the microwave signals utilizing optical heterodyne techniques. The optical heterodyne receiver

creates a difference frequency within the bandwidth of the detector and shifts the desired microwave signals to that frequency as a result of the optical mixing. This latter case applies to the system wherein multiple optical carriers are used to transmit higher frequency microwave signal components. The RF/microwave analog of the heterodyne receiver applies in the case where a single optical carrier is utilized to transmit multiple high frequency microwave subcarriers.

10 The advantages of this invention result in significant cost savings to the network provider by enabling bandwidth upgrades while maximizing the utilization of existing terminal equipment on the network. For example, consider the case where a telecom provider may wish to upgrade a metropolitan network from 622 Mbps (OC-12) to 9.952 Gbps (OC-192). The prior art would require the replacement of all OC-12 terminal equipment with OC-48 terminal equipment at a significant cost to the network provider. Conversely 20 this invention enables the utilization of the existing OC-12 infrastructure while increasing the network bandwidth to the equivalent of an OC-192 without the need for conventional WDM techniques. Considering the fact that the cost of the OC-192 terminal equipment is substantially greater than that of the OC-12 equipment, 25 the cost benefits of this approach are clear and apply at every terminal where the full OC-192 bandwidth is not required. Application of conventional WDM techniques to increase the number of OC-12 optical carriers are similarly cost prohibitive in contrast to 30 the invention described herein.

The fact that this invention enables the bandwidth to be remotely selected introduces the additional utility of bandwidth mobility. Thus the bandwidth delivered to any particular point on the network can be
5 remotely adjusted to accommodate actual demand. In other words, if a portion of the network is not too busy, multiple nodes in that area can be served by the a single microwave subcarrier by simply tuning the voltage controlled oscillators (VCO's) that select the
10 microwave band to the same frequency at each of several nodes. The available bandwidth can be concentrated over a different portion of the network where demand is higher by tuning all of the VCO's in the busy area to different frequencies. Later as loading shifts, the VCO
15 tuning can be adjusted to accommodated the change in network loading conditions.

The method described herein applies to RF/microwave carriers that reside on a single optical wavelength or multiple optical wavelengths. In the case
20 where multiple optical wavelengths are utilized, the method further includes the steps of controlling the wavelengths of the optical carriers. Thus the demodulation is accomplished relative to a stable optical frequency.

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Brief Description of the Drawings

FIG. 1 illustrates an embodiment of the invention applied specifically to the CATV distribution network architecture utilizing SCM techniques to transmit a
30 combination of AM-VSB and digital QAM signals. This preferred embodiment employs analog subcarrier

frequencies in the RF range below 700 MHz to transmit the digital QAM signals over the fiber.

FIG. 2 extends the architecture depicted in FIG. 1 by utilizing more of the optical bandwidth by
5 incorporating analog carriers up to 2.0 GHz for transmitting the digital QAM signals.

FIG. 3 depicts the network architecture in accordance with a preferred embodiment as it applies to a fiber optic telecommunications network in general.
10 Note that this is an asymmetrical network architecture wherein the transmitter bandwidth exceeds that of the receiver. This generalization of the network architecture is pertinent to digital communications signals (e.g. TDM of amplitude shift keyed binary data)
15 such that the final stage of demodulation is baseband.

FIG. 4 depicts the heterodyne system in the logical extension of an illustrated embodiment to higher bandwidth where the demultiplexing of multiple optical carrier frequencies is accomplished by
20 incorporating an optical mixer to create an optical beat note by shifting the desired part of the microwave carrier spectrum into the bandwidth of the receiver.

FIG. 5 depicts a polarizing alignment device under an illustrated embodiment which eliminates polarization
25 dependent loss in the system while enabling distribution of the local oscillator laser power to multiple nodes of the network.

FIG. 6 depicts the polarization alignment device in the optional embodiment wherein a single mode fiber
30 terminates the system after the linear polarization state has been recovered, establishing an unknown (and

dynamic) state of elliptical polarization at the receiver.

FIG. 7 depicts the polarization alignment device in the optional embodiment wherein a single mode fiber coupler is used to combine the signal and local oscillator laser fields and a single mode fiber transmission line is used to deliver the signal and local oscillator fields in independent and arbitrary polarization states to the polarization recovery device.

FIG. 8 depicts the optical frequency plan whereby a single optical carrier may be utilized to carry four sets of microwave subcarriers. FIG. 8a shows the optical spectrum indicating independent communications signal applied to the upper and lower sidebands of the optical and microwave carriers respectively. FIG. 8b shows the local oscillator wavelength that is utilized to demodulate the lower frequency set (i.e., the lower optical sideband). FIG. 8c shows the local oscillator wavelength that demodulates the higher frequency set.

Detailed Description of a Preferred Embodiment

FIG. 1 shows a simplified schematic of a transmitter/receiver 10 as it applies to the CATV network architecture. In this embodiment, the CATV broadcast signals are transmitted by a laser transmitter 12 on a first optical carrier and occupy the RF bandwidth from 50-550 MHz. Multiple bands of RF signals are transmitted by a second laser transmitter 14 on the second optical carrier and occupy the RF bandwidth from 0.1-700 MHz. The optical carriers may be produced by high linearity DFB lasers (e.g. Lucent

Technologies model 257). The two optical carriers are combined at the first passive optical hub 16 and thereafter may be distributed to several opto-electronic nodes (one node 18 is illustrated in FIG.

5 1).

Each opto-electronic node 18 contains an optical filter 20 (to separate the two optical wavelengths) and two optical receivers 24, 26 (one for each optical wavelength). The filter 20 passes the first optical carrier to the first receiver 24 and reflects the second carrier. The reflection causes the second carrier to travel back through the optical recirculator 22 to the second receiver 26.

Within the second receiver 26, the second carrier is detected in a detector 28 and amplified in an amplifier 30. An RF/microwave mixer 34 (e.g. such as manufactured by Watkins-Johnson) utilizes a tunable RF oscillator 32 (e.g. Avantek VCO) to select one 200 MHz band from the 700 MHz transmission and shift the center frequency of that selected band to 650 MHz. Thus, the selected 200 MHz band occupies the bandwidth from 550-750 MHz. Any low frequency components of the IF output from the mixer 34 are filtered by a high pass filter 36. Such high pass filter 36 comprises a component of a diplexer, the low-pass component 38 of which passes the 50-550 MHz SCM analog AM-VSB transmission.

The first receiver 24 detects the first carrier in a detector 40. An amplifier 42 amplifies the signal which may then be applied to the low-pass component 38 of the diplexer. The diplexer functions to combine the selected 200 MHz band with the SCM AM-VSB signal. A broadband amplifier 44 amplifies and then distributes

the 50-550 MHz broadcast signal along with the selected 200 MHz band of QAM signals over the coaxial cable network (not shown).

It should be noted that in the architecture depicted in FIG. 1, the illustrated embodiment shows the channels in the bandwidth below 700 MHz that are readily available to the CATV network operator at the head-end. However the invention as depicted in FIG. 1 is also pertinent to higher frequency transmissions, for example utilizing a 1.2 GHz bandwidth between 0.8 and 2.0 GHz. In this case more bandwidth is available but the bandwidth below 800 MHz is not used.

The bandwidth limitation arises due to the fact that the IF output from the mixer comprises sum and difference frequencies of the LO and RF frequencies. The situation must be avoided where difference frequencies of one detected band can occur at the same frequency as the sum frequencies from another band. Ultimately, by increasing utilization of spectrum into L-band, a frequency is reached that will result in a difference frequency of 800 MHz that occurs within desired 550-750 MHz band (i.e. when the LO frequency is equal to 1350 MHz). Therefore the highest carrier frequency pertinent to the architecture of FIG. 1 would be 2.1 GHz.

The illustrated embodiment utilizes the spectrum below 700 MHz that is readily available to the network operator. This is consistent with a primary objective of the invention in order to maximize utilization of existing terminal equipment. Nevertheless, it may be desirable to utilize more of the available bandwidth on a given optical carrier at the same time. A

modification of the network architecture to enable maximum utilization of the laser bandwidth is shown in FIG. 2.

The CATV network depicted by FIG. 2 could
5 potentially use all of the available modulation spectrum on a single wavelength. In the example shown a 2000 MHz transmission is implemented within the second transmitter 100. This is well within the modulation bandwidth for direct modulation of the DFB laser
10 junction. To avoid the bandwidth limitations described above, the embodiment of FIG. 2 implements a two stage mixing process. The first stage mixer 102, in combination with a bandpass filter 106, selects the desired 200 MHz band from the transmission and the
15 second mixer 104 shifts that band into the desired 550-750 MHz spectrum.

The selection is accomplished by upconversion of the desired 200 MHz bandwidth within the first mixer 102 to a frequency greater than 2.0 GHz (e.g. 2.4 GHz).
20 The bandpass filter 106 separates the 200 MHz band from the multiple detected frequency bands. After filtering the desired band, a tuned RF oscillator 108 drives the second mixer 104 LO input and thereby tunes the center frequency of the selected band to the appropriate RF
25 frequency, in this case 650 MHz. An RF diplexer 110 thereafter combines the selected 200 MHz band with the 50-550 MHz broadcast signal. The broadband amplifier 112 then distributes the 50-550 MHz broadcast signal along with the selected 200 MHz band over the coaxial
30 cable network connected thereto.

The network topologies described above are specifically applicable to the SCM transmission

characteristic of the CATV network. However much of the digital telecommunications infrastructure utilizes TDM techniques to carry amplitude shift keyed (ASK) modulation of binary signals. These systems typically
5 operate at baseband, in contrast to the SCM techniques common in the CATV network architecture. Notwithstanding such differences, the general embodiment of this invention for ASK, FSK, or PSK modulation formats provides substantial benefits to the
10 binary digital network operating at baseband.

FIG. 3 illustrates an embodiment of the invention that may be particularly applicable to telecommunications network topologies that utilize TDM techniques to multiplex binary modulation signals such
15 as ASK. This is a natural extension of the network topology discussed above and it could be successfully applied to SCM signals (provided that operation at baseband is desired). However the network depicted in FIG. 3 does not accommodate the integration of
20 broadcast signals with the SCM digital transmission.

Let us consider the topology of FIG. 3 wherein a high frequency laser transmitter is utilized to distribute multiple lower frequency digital TDM signals. For example an externally modulated 1550 nm
25 DFB laser (e.g. Fujitsu FLD5F6CX utilized with a 10 Gbps modulator manufactured by Uniphase Telecommunications Products) may be incorporated to transmit 16 OC-12 signals over a fiber optic network.

FIG. 3 details the circuit arrangement that may be
30 utilized to combine multiple OC-12 or OC-192 signals. (Note that such a circuit arrangement could be applied to the 2.0 GHz transmission of digital QAM subcarriers

described in regard to FIG. 1 by multiplexing ten 200 MHz bandwidth SCM based QAM signals. It is also feasible that the QAM signals may be directly modulated on individual analog carriers up to 2.0 GHz.

5 Furthermore, the externally modulated DFB laser described above may be utilized to increase the bandwidth of the QAM subcarrier frequencies substantially above 2.0 GHz in the CATV network application.)

10 The transmitter circuit of FIG. 3 utilizes several different oscillator frequencies (f_1 -- f_N) to tune the individual OC-12, OC-192 or QAM channels to different microwave carrier frequencies that are subsequently combined by the bandpass filter based multiplexing
15 network 200. The multiplexed communications signals are propagated through a fiber network 202 that may contain optical splitters and optical amplifiers in order to distribute the multiplexed signal to multiple nodes 204 on the network.

20 The high frequency receiver at any given node 204 will detect the entire spectrum of microwave subcarriers and select an individual SCM channel with a VCO based band selector in a manner analogous to that of the CATV receiver described in connection with FIG.

25 2 above. But in this case, the new IF frequency is shifted to a higher microwave frequency since the highest microwave subcarriers may be above 10 GHz. There is another distinct contrast between the node architectures of FIGs. 2 and 3 as indicated above.

30 Whereas in FIG. 2 the second mixer stage 206 centers the selected band at 650 MHz, the selected channel in FIG. 3 is tuned to baseband.

As the frequency of the microwave subcarriers is increased above 10-20 GHz, it becomes practically much more difficult to implement the architecture depicted in FIG. 3 due to the high microwave frequencies
5 involved. Thus it becomes desirable to utilize optical techniques in order to manage the communications signals at higher frequency microwave subcarriers.

The architecture depicted in FIG. 4 utilizes multiple optical wavelengths to carry the transmission.
10 The transmitter 400 containing the multiple optical sources 401-403 is indicated as the optical channel bank 404. The significant increases in bandwidth made possible by the optically multiplexed transmission reduce the feasibility of utilizing an IF frequency
15 that is above the highest microwave frequency component of the optical transmission. Therefore the optical demultiplexing topology of FIG. 4 incorporates optical heterodyne detection techniques.

In order to realize IF frequencies within the
20 communications bandwidth, adjacent optical frequencies are separated by adequate microwave bandwidth to accommodate the signal bandwidth shifted by a heterodyne difference frequency. The difference frequency thus comprises a fraction of the optical
25 frequency spacing.

Multiple transmitter lasers 401-403 are utilized in this embodiment, each of which may carry a SDM microwave spectrum (or a single high frequency TDM transmission). Each laser is stabilized to a known
30 optical frequency referenced to the fiber optic resonator 406. Feedback electronics are utilized to control the free spectral range of the fiber resonator

406 by controlling its temperature, and the absolute wavelength of each respective laser 401-403 is controlled by feedback to its respective injection current control. The various feedback signals are
5 derived at different frequencies and the bandpass filter network demultiplexes these signals and directs each one to the appropriate laser control circuit.

The free spectral range of the fiber optic resonator 406 is locked to a microwave frequency and
10 the WDM lasers 401-403 are locked to known optical frequencies referenced to that resonator 406. One such known optical frequency (i.e., mode) is referenced to an absolute optical frequency and all other mode numbers are determined relative to the absolute optical
15 frequency. The generation of the absolute optical frequency and the locking of the free spectral range may be accomplished as described in U.S. Patent No. 5,717,708 issued in the name of the present inventor, and using the techniques described by Hall (*Optical*
20 *Heterodyne Saturation Spectroscopy*, Hall et al., Appl. Phys. Lett., Nov. 1981) to lock this reference laser to an absolute optical frequency reference (e.g., rubidium) and/or the technique described by DeVoe and Brewer to stabilize and lock the free spectral range of
25 the optical reference resonator to a known microwave frequency.

Alternatively, each of the WDM lasers 401-403 may simply be calibrated to its own known optical frequency (each with its own line-narrowing resonator 406). The
30 prior art has taught a number of methods of determining known optical frequencies (e.g., wavemeters based upon Michelson interferometers, other types of

interferometers based upon diffraction gratings, etc.). Other newer methods may also be used such as molecular resonance cells (e.g., rubidium cells for stabilizing a single known frequency, resonance vibration cells
5 including acetylene cells which may be used to provide a multitude of reference frequencies, etc.).

The laser wavelengths of WDM lasers 401-403 are combined through a standard WDM multiplexing technique (e.g. the combination of optical circulators 408, 410
10 and fiber Bragg gratings 412, 414). A small sample of the WDM spectrum may be incident upon the fiber resonator 406 and the reflection is utilized as a feedback signal in order to derive the appropriate control signals. The majority of the WDM power output
15 is transmitted through the single mode fiber network 416.

FIG. 4 further depicts a tunable local oscillator (LO) laser 418 that may be used to select a single transmitter laser frequency through the network 416
20 from the optical channel bank 404. This laser 418 is also referenced to an optical resonator, the free spectral range of which is also locked to a microwave oscillator. However the free spectral range of the LO based resonator is an integral fraction of the optical
25 channel spacing (e.g. a factor of not less than three). Furthermore the microwave bandwidth on each optical carrier is chosen to be less than the free spectral range of the LO based resonator. In order to select a microwave band from the optically multiplexed
30 transmission, the LO signal is locked to a mode of that resonator that is adjacent to the mode at which the desired signal wavelength is resonant. The LO laser

418 may be constructed substantially as described in U.S. Patent No. 5,717,708 issued in the name of the present inventor.

The receiver of FIG. 4 functions by introducing a local oscillator (LO) laser signal in the vicinity of, but not necessarily at, the physical location of the node 422, 424. In fact this design (FIG. 5) shows the LO laser power shared between two nodes 422, 424. The polarization alignment device comprises a polarization beamsplitter 426 and a 50% PM fiber coupler 428. The input PM fiber 430 from the LO 418 may be rotated 45° so that equal components of LO power excite both polarization axes. Both output polarizations are aligned to the same polarization axis of the PM fibers (e.g. the slow axis). One of the PM fibers 432 is rotated 90° so that a single polarization is coupled in the 50% PM fiber coupler 428. Although the signal input is arbitrarily polarized, the 50% fiber coupler 428 and 90° rotation of one of the PM fibers 432 ensures that equal components of signal power will propagate along both outputs of the beam polarization alignment device. As used herein, rotation means twisting one end of the PM fibers relative to the other end.

The polarization alignment thus ensures that the LO and signal fields are in a common state of polarization. Furthermore, once the polarization of the local oscillator (LO) laser is matched to that of the received laser, it becomes possible to reestablish the transmission in single mode fiber so that one or both of the nodes can be remotely located. Although the beam will once again become depolarized, the unknown state

of elliptical polarization will be matched for both the LO and received laser beams.

A heterodyne difference frequency is detected in detectors 438, 440 of the tuned receivers 422, 424. A
5 final stage microwave demodulation within mixers 434, 436 returns the communications signal to baseband. This final mixer stage 434, 436 also serves to select one of the two sets of microwave subcarriers that are detected by detectors 438, 440 within the bandwidth of the
10 bandpass filter of the tuned receiver. Thus each optical wavelength can carry up to four sets of microwave subcarriers (FIG. 8a). The lower frequency set is chosen by tuning the LO laser to the LO resonator mode below the desired carrier (FIG. 8b).
15 Conversely the higher frequency set is chosen by tuning the LO laser to the LO resonator mode above the desired carrier (FIG. 8c).

FIG. 6 depicts an implementation of the invention in a coherent optical communications link wherein a
20 single mode fiber is utilized to distribute the local oscillator laser and single laser power to the receiver without incurring polarization dependent loss due to the depolarizing properties of the single mode fiber. In order to accomplish this desired effect, it is
25 necessary first to utilize a polarization preserving system (e.g., Panda fiber) to align the signal and local oscillator laser polarization to a common linear state. Once a common linear state is achieved, that state can be altered into any arbitrary state, without
30 incurring polarization dependent loss provided that such an arbitrary state is precisely matched for the

optical polarization of both signal and local oscillator laser fields.

One method of accomplishing this effect, as is depicted in FIG. 6, is to splice the Panda fiber to the single mode fiber utilizing a fusion splicer. In such an implementation, the Panda fiber will ensure that the same linear polarization state is launched into the single mode fiber for both signal and local oscillator lasers. The polarization mode dispersion will not cause polarization dependent loss because both signal and local oscillator fields remain in the same arbitrary state of polarization through the depolarizing fiber. In this manner, the benefits of the coherent optical system can be applied to the optical network utilizing standard single mode fiber which enabling distribution of the optically demodulation single power to multiple nodes of the fiber network.

In fact, the polarization restoring device is insensitive to the state of input polarization so that the device could function just as well to restore a common polarization to two input fields of arbitrary polarization states. (Note that the local oscillator laser input fiber to the polarization restoring device in FIG. 4 is indicated to be optionally a single mode fiber or polarization maintaining fiber. Also the rotation of the polarization maintaining fiber at the input to the polarization is entirely arbitrary.)

FIG. 7 depicts an illustrated embodiment wherein the signal and local oscillator laser fields are mixed within a single mode fiber so that the two fields are in arbitrary and independent polarization states at the input to the polarization recovery device. In this

case only a single input fiber is required and the two fields are independently restored to a linear polarization state by the optics.

Thus it becomes apparent that the optical
5 heterodyne techniques described above and depicted in FIG. 4 are a direct extension of the microwave mixing techniques discussed with regard to FIGs. 1-3. All of these techniques are pertinent to increasing bandwidth utilization on the network while maintaining
10 substantially more flexibility and achieving considerably more cost effective deployment than that afforded by conventional WDM techniques. Furthermore, even in the most advanced implementations of the coherent optical heterodyne system, the system
15 deployment in general does not cause the obsolescence of the existing terminal equipment infrastructure.

A specific embodiment of a method and apparatus for modulating a coherent beam according to the present invention has been described for the purpose of
20 illustrating the manner in which the invention is made and used. It should be understood that the implementation of other variations and modifications of the invention and its various aspects will be apparent to one skilled in the art, and that the invention is
25 not limited by the specific embodiments described. Therefore, it is contemplated to cover the present invention and any and all modifications, variations, or equivalents that fall within the true spirit and scope of the basic underlying principles disclosed and
30 claimed herein.